

Fluid Dynamics Key Equations

Steady Streamlines

For a two-dimensional velocity field:

$$\vec{u}(x, y) = u(x, y)\hat{i} + v(x, y)\hat{j}$$

The streamlines are:

$$\int \frac{1}{v(x, y)} dy = \int \frac{1}{u(x, y)} dx$$

Forces in Fluids

Shear Stress, τ

$$\tau = \frac{F}{A}$$

$$\tau = \mu \frac{du}{dy}$$

Fluid Statics

Hydrostatic

$$\frac{dP}{dz} = -\rho g$$

Equation

$$\Delta P = -\rho g \Delta z$$

Resultant Pressure Force

$$F_R = \int P dA$$

$$F_R = \int_A \rho g y dA$$

Point of Application

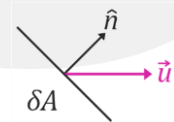
$$y' = \frac{\int_A P y dA}{\int_A P dA}$$

$$y' = \frac{\int y^2 dy}{\int y dy}$$

- dA must be a function of y

Mass Flow Rate

Vectorial



$$\dot{m} = \int_A \rho \vec{u} \cdot d\vec{A}$$

Perpendicular \vec{u}

$$\dot{m} = \rho u A$$

Unsteady Streamlines & Pathlines

For a two-dimensional unsteady field:

$$\vec{u}(x, y, t) = u(x, y, t)\hat{i} + v(x, y, t)\hat{j}$$

The parametrised pathlines are:

$$x = \int u(x, y, t) dt \quad y = \int v(x, y, t) dt$$

Pressure Force

$$F_P = PA$$

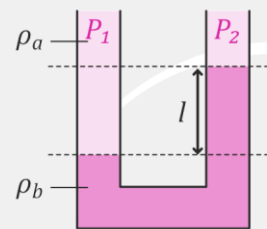
Viscous Force

$$F_V = \tau A = \mu \frac{du}{dy} A$$

Kinematic Viscosity, ν

$$\nu = \frac{\mu}{\rho}$$

Manometer



$$P_2 - P_1 = gl(\rho_a - \rho_b)$$

Archimedes' Principle & Buoyancy

"The magnitude of upthrust is equal to the weight of water displaced"

Reynold's Transport Theorem

$$\frac{d}{dt} \int_{V_{sys}(t)} \eta \rho dV = \frac{d}{dt} \int_{CV} \eta \rho dV + \int_{CS} \eta \rho \vec{u} \cdot d\vec{A}$$

Rate of change of N in the system

Rate of change of N in the CV and system

Net flow rate of N out of the CV

- N is the property being conserved, $N = \eta m$
- $\rho \eta$ is the property N per unit volume

Conservation of Mass

$$\underbrace{\frac{d}{dt} \int_{CV} \rho dV}_{\text{Rate at which the CV gains mass}} = - \underbrace{\int_{CS} \rho \vec{u} \cdot \vec{dA}}_{\text{Net flow rate of mass out of the CV}}$$

Rate at which the CV gains mass

Net flow rate of mass out of the CV

Algebraic Formulation

$$\frac{dm}{dt} = \sum \dot{m}_{in} - \sum \dot{m}_{out}$$

Steady Flow

$$\sum \dot{m}_{in} = \sum \dot{m}_{out}$$

$$\int_{CS} \rho \vec{u} \cdot \vec{dA} = 0$$

Steady, uniform flow with constant density

$$\sum uA_{in} = \sum uA_{out}$$

Conservation of Momentum

$$\sum \vec{F} = \frac{d}{dt} \int_{CV} \vec{u} \rho dV + \int_{CS} \vec{u} \rho \vec{u} \cdot \vec{dA}$$

Steady Flow

$$\sum \vec{F} = \int_{CS} \vec{u} \rho \vec{u} \cdot \vec{dA}$$

Steady resolved components

Flow, into

$$\sum F_x = \int_{CS} u_x \rho \vec{u} \cdot \vec{dA}$$

$$\sum F_y = \int_{CS} v_y \rho \vec{u} \cdot \vec{dA}$$

- Because $N = M = m\vec{u}$, so $\eta = \vec{u}$

Steady, uniform, constant density

$$\sum F_x = \sum_{out} \dot{m}u - \sum_{in} \dot{m}u$$

$$\sum F_y = \sum_{out} \dot{m}v - \sum_{in} \dot{m}v$$

With Conservation of Mass for one inlet and outlet

$$\sum F_x = \dot{m}(u_{out} - u_{in})_x$$

$$\sum F_y = \dot{m}(v_{out} - v_{in})_y$$

The Bernoulli Equation

$$\frac{P_1}{\rho} + \frac{1}{2}u_1^2 + gz_1 = \frac{P_2}{\rho} + \frac{1}{2}u_2^2 + gz_2 = c$$

This assumes:

- Steady flow
- Inviscid Flow
- Incompressible (constant ρ) flow
- Two points are on the same streamline/ have the same Bernoulli constant

Conservation of Energy for Steady Flow

$$\dot{Q} - \dot{W} = \int_{CS} \left(\frac{P}{\rho} + \frac{1}{2}u^2 + gz + e \right) \rho \vec{u} \cdot \vec{dA}$$

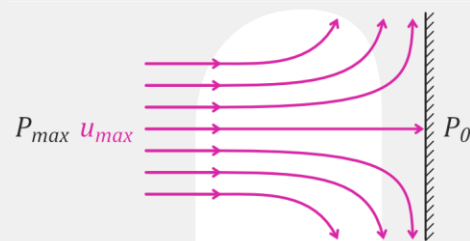
1st Thermo Law

$$\frac{dE_{sys}}{dt} = \dot{Q} - \dot{W}$$

Derived from RTP

$$\eta = \frac{1}{2}u^2 + gz + e$$

Stagnation Point Flow



$$\frac{P_{max}}{\rho} + \frac{1}{2}u_{max}^2 = \frac{P_0}{\rho}$$

For a uniform velocity profile:

$$q - w = \Delta \left(\frac{P}{\rho} + \frac{1}{2}u^2 + gz + e \right)$$

The Pipe Flow Energy Equation (PFEE)

$$\frac{P_1}{\rho} + \frac{1}{2}u_1^2 + gz_1 = \frac{P_2}{\rho} + \frac{1}{2}u_2^2 + gz_2 + w_L - w_P$$

- w_L is the lost energy
- $w_P = w$ is the pump work

$$\frac{P_1}{\rho g} + \frac{1}{2g}u_1^2 + z_1 = \frac{P_2}{\rho g} + \frac{1}{2g}u_2^2 + z_2 + h_L - h_P$$

- h_L is the lost head
- h_P is the pump head

Laminar Flow between Horizontal Plates

$$u(y) = -\frac{h^2 \Delta P}{2\mu L} \left(1 - \frac{y^2}{h^2}\right)$$

Where u_{max} equals $-\frac{h^2 \Delta P}{2\mu L}$

Turbulent Flow in Circular Pipes

Reynold's Number, Re $Re = \frac{\rho u d}{\mu} = \frac{u d}{\nu}$

Mean Velocity, u $u = \frac{Q}{A}$

Lost Head

Lost head, h_L $h_L = h_f + h_l$

Major Losses, h_f $h_f = f \frac{Lu^2}{2dg}$

Minor Losses, h_l $h_l = k \frac{u^2}{2g}$

The pipe flow energy equation only applies for flow that is:

- Steady
- Adiabatic
- Incompressible
- Uniform velocity field
- Between a single inlet and outlet

Laminar Flow in a Circular Pipe

$$u(r) = -\frac{R^2 \Delta P}{4\mu L} \left(1 - \frac{r^2}{R^2}\right)$$

Where u_{max} equals $-\frac{R^2 \Delta P}{4\mu L}$

Friction Factor, f $f = \frac{Re}{64}$

Relative roughness, r $r = \frac{\epsilon}{D}$

Pump Head

Pump head, h_P $h_P = \frac{W_P}{g}$

$$h_P = \frac{\dot{W}_P}{\dot{m}g}$$

$$h_P = \frac{\Delta P_P}{\rho g}$$